

# Analysis of Statically Indeterminate Structures Using the Force Method

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# Statically Indeterminate Structures

At the beginning of the course, we learned that a **stable structure** that contains **more unknowns than independent equations of equilibrium** is **Statically Indeterminate**.

## Advantages

- Redundancy (several members must fail for the structure to become unstable);
- Often maximum stresses in certain members are reduced;
- Usually deflections are reduced.

## Disadvantages

- Connections are often more expensive;
- Finding forces and deflections using hand analysis is much more complicated.

# Steps in Solving an Indeterminate Structure using the Force Method

Determine degree of Indeterminacy  
Let  $n$  = degree of indeterminacy  
(i.e. the structure is indeterminate to the  $n$ th degree)

Chapter 3

Define Primary Structure and the  $n$  Redundants

Define the Primary Problem

Solve for the  $n$  Relevant Deflections in Primary Problem

Chapters 3,4,5 then 7 or 8

Define the  $n$  Redundant Problems

Solve for the  $n$  Relevant Deflections in each Redundant Problem

Chapters 3,4,5 then 7 or 8

Write the  $n$  Compatibility Equations at Relevant Points

Solve the  $n$  Compatibility Equations to find the  $n$  Redundants

Chapter 3

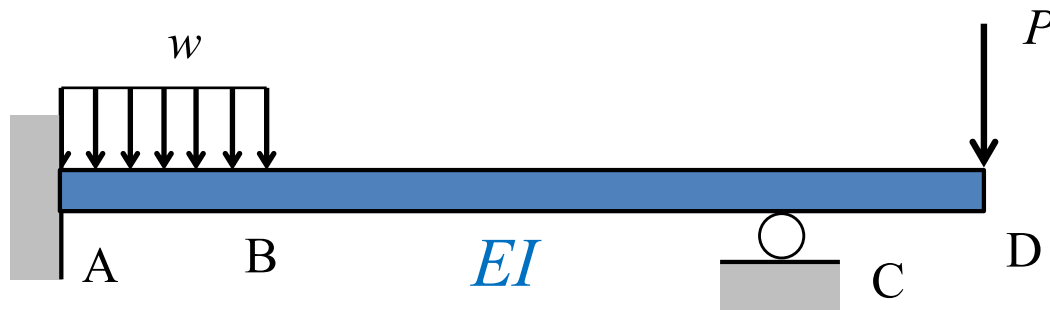
Use the Equations of Equilibrium to solve for the remaining unknowns

Construct Internal Force Diagrams (if necessary)

Chapters 3,4,5

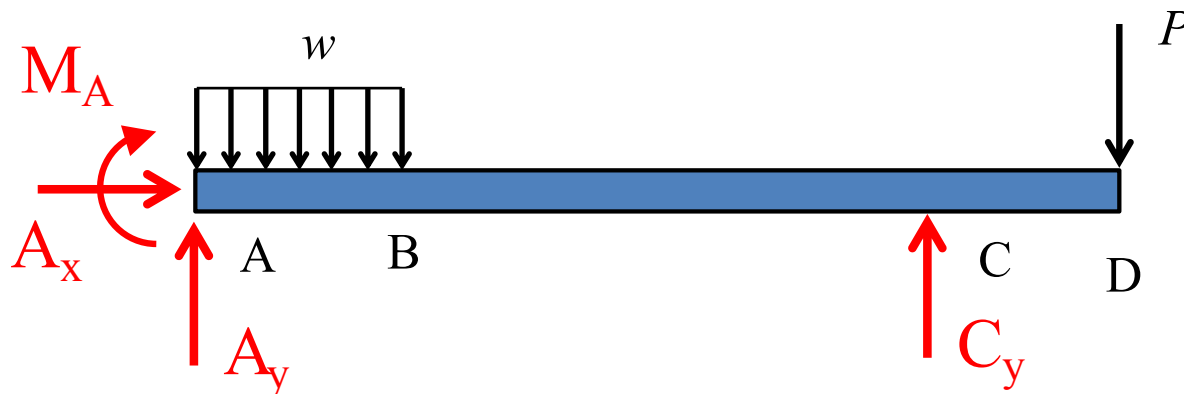
# Force Method of Analysis

Consider the beam



Beam is stable

FBD



$$X = 4$$

$$3n = 3(1) = 3$$

Statically Indeterminate to the 1<sup>st</sup> degree

# Define Primary Structure and Redundants

- Remove all applied loads from the actual structure;
- Remove support reactions or internal forces to define a primary structure;
- Removed reactions or internal forces are called redundants;
- Same number of redundants as degree of indeterminacy
- Primary structure must be stable and statically determinate;
- Primary structure is not unique – there are several choices.

**Primary Structure**

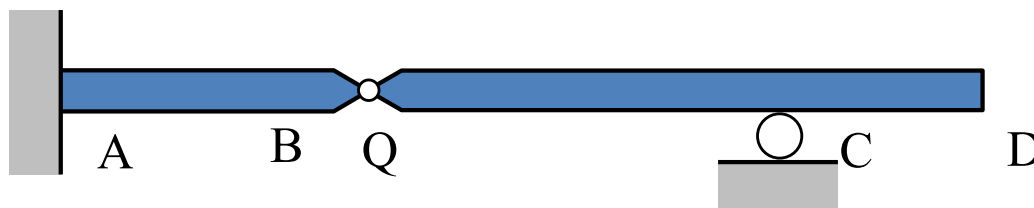
**Redundant**



$M_A$



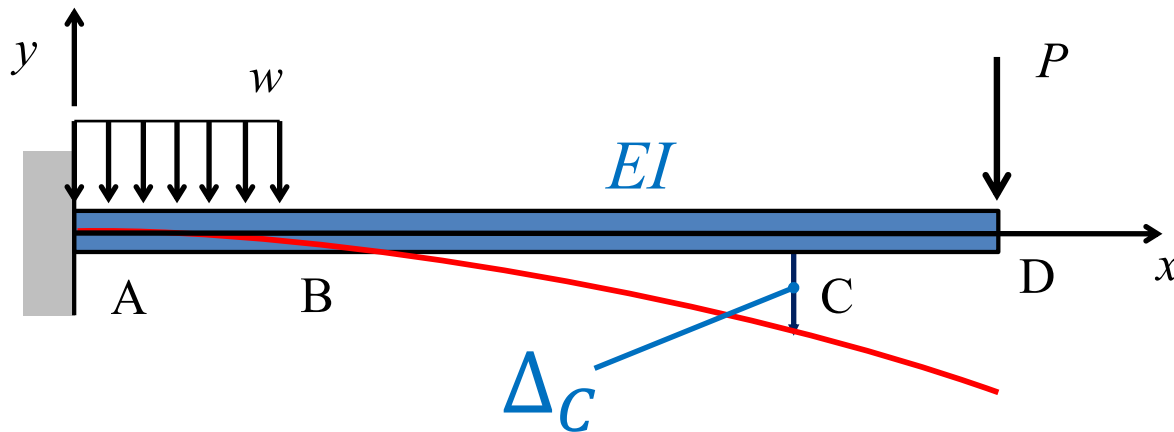
$C_y$



$M_Q$

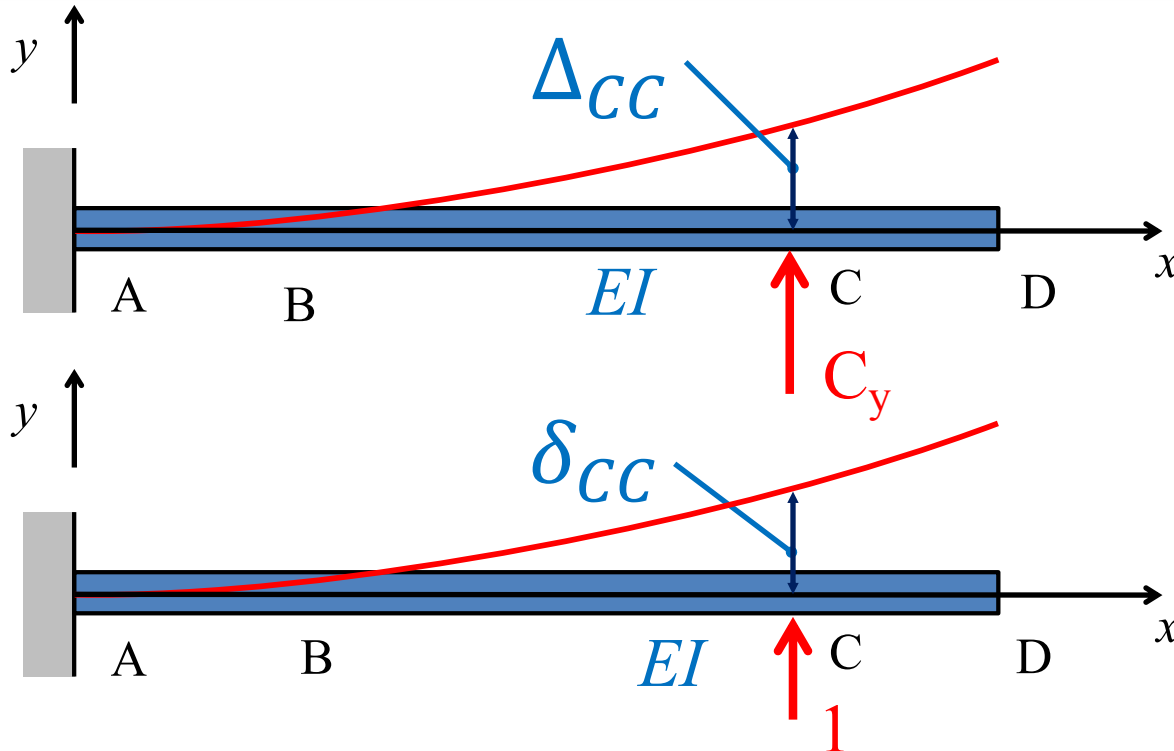
# Define and Solve the Primary Problem

- Apply all loads on actual structure to the primary structure;
- Define a reference coordinate system;
- Calculate relevant deflections at points where redundants were removed.



# Define and Solve the Redundant Problem

- There are the same number of redundant problems as degrees of indeterminacy;
- Define a reference coordinate system;
- Apply only one redundant to the primary structure;
- Write the redundant deflection in terms of the flexibility coefficient and the redundant for each redundant problem.
- Calculate the flexibility coefficient associated with the relevant deflections for each redundant problem;



**Redundant Problem**

$$\Delta_{CC} = C_y \delta_{CC}$$

# Compatibility Equation

## Compatibility at Point C

$$\Delta_C + \Delta_{CC} = 0$$

$$\Delta_C + C_y \delta_{CC} = 0$$

Solve for  $C_y$



# The Force Method is Based on the Principle of Superposition

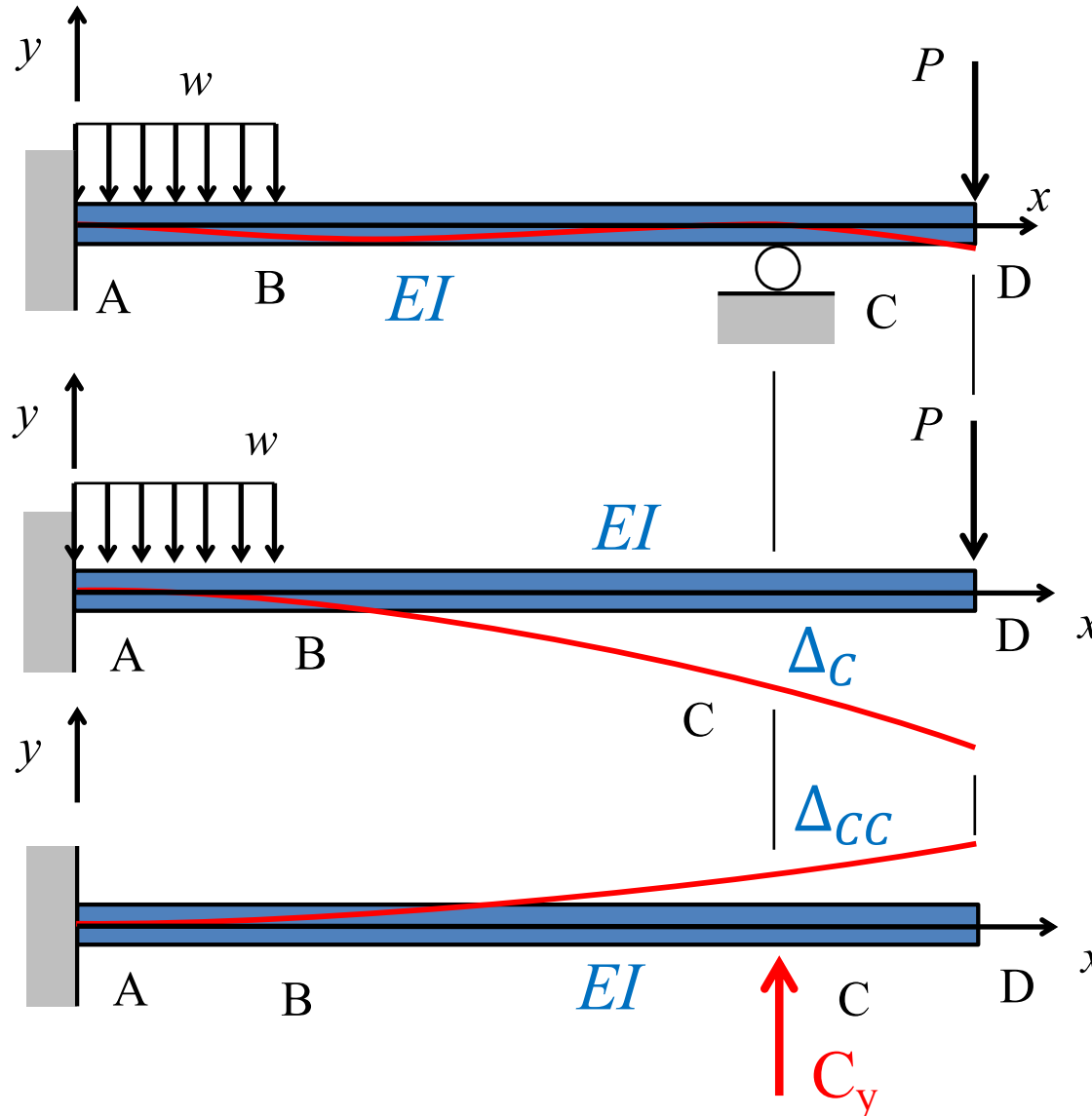
Indeterminate Problem

=

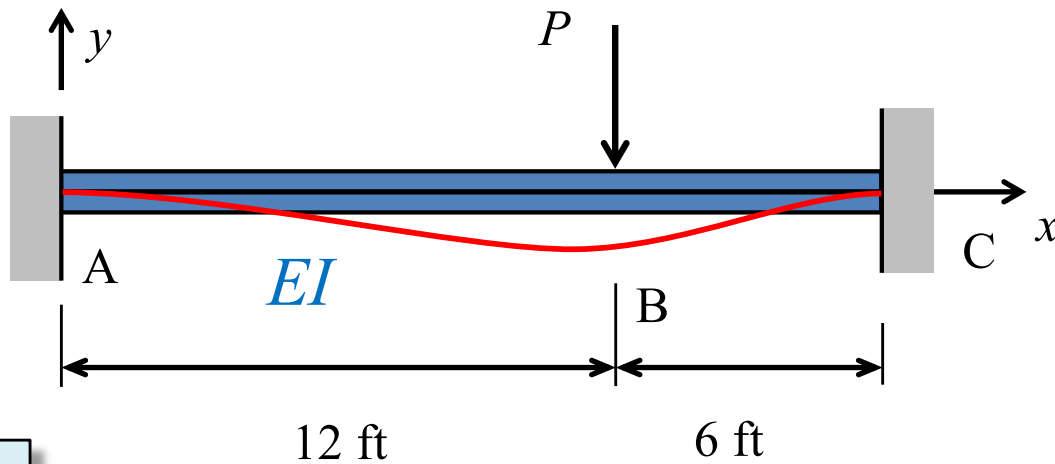
Primary Problem

+

Redundant Problem

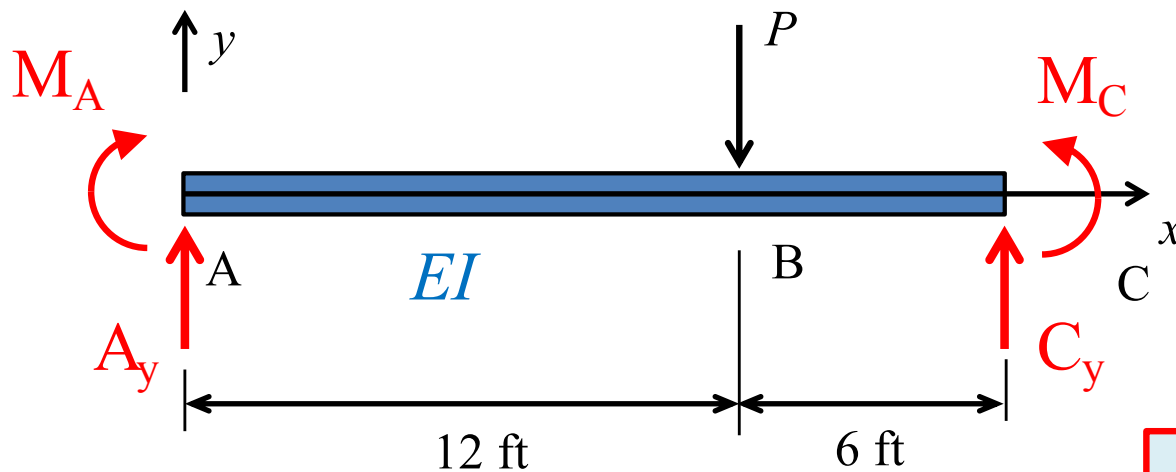


# Lab Problem



For the indeterminate beam from Lab 11, subject to the point load at B, find the support reactions at A and C and construct the shear and moment diagram for the beam. Neglect axial force effects.

FBD



Beam is stable

4 unknowns

2 equations of equilibrium

Statically Indeterminate to the 2<sup>nd</sup> degree

# Define Primary Structure and Redundant

- Remove all applied loads from the actual structure;
- Remove support reactions or internal forces to define a primary structure;
- Removed reactions or internal forces are called redundants;
- Same number of redundants as degree of indeterminacy
- Primary structure must be stable and statically determinate;
- Primary structure is not unique – there are several choices.

**Primary Structure**

**Redundants**



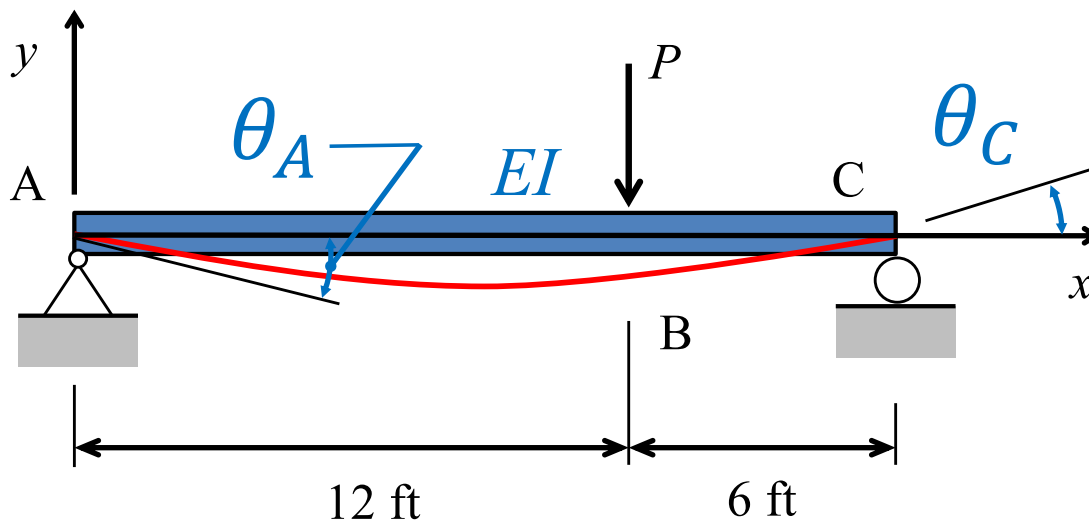
$M_C$     $C_y$



$M_A$     $M_C$

# Define and Solve the Primary Problem

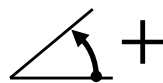
- Apply all loads on actual structure to the primary structure;
- Define a reference coordinate system;
- Calculate relevant deflections at points where redundants were removed.



**From  
Tabulated  
Solutions**

$$\theta_A = ??$$

$$\theta_C = ??$$



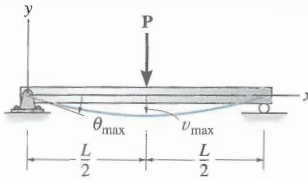
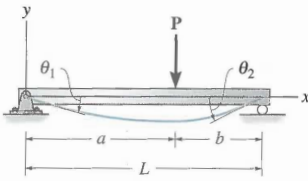
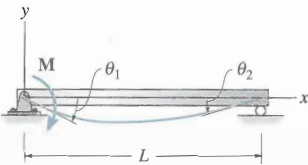
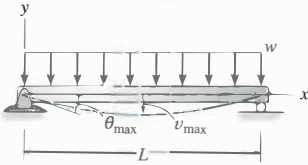
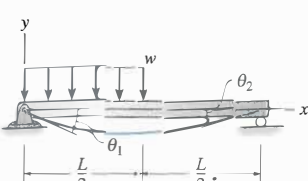
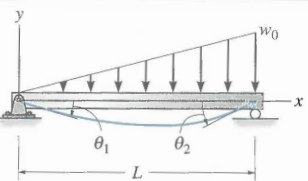
Counter-clockwise  
rotations positive

# Tabulated Solutions

$$v \quad + \uparrow$$

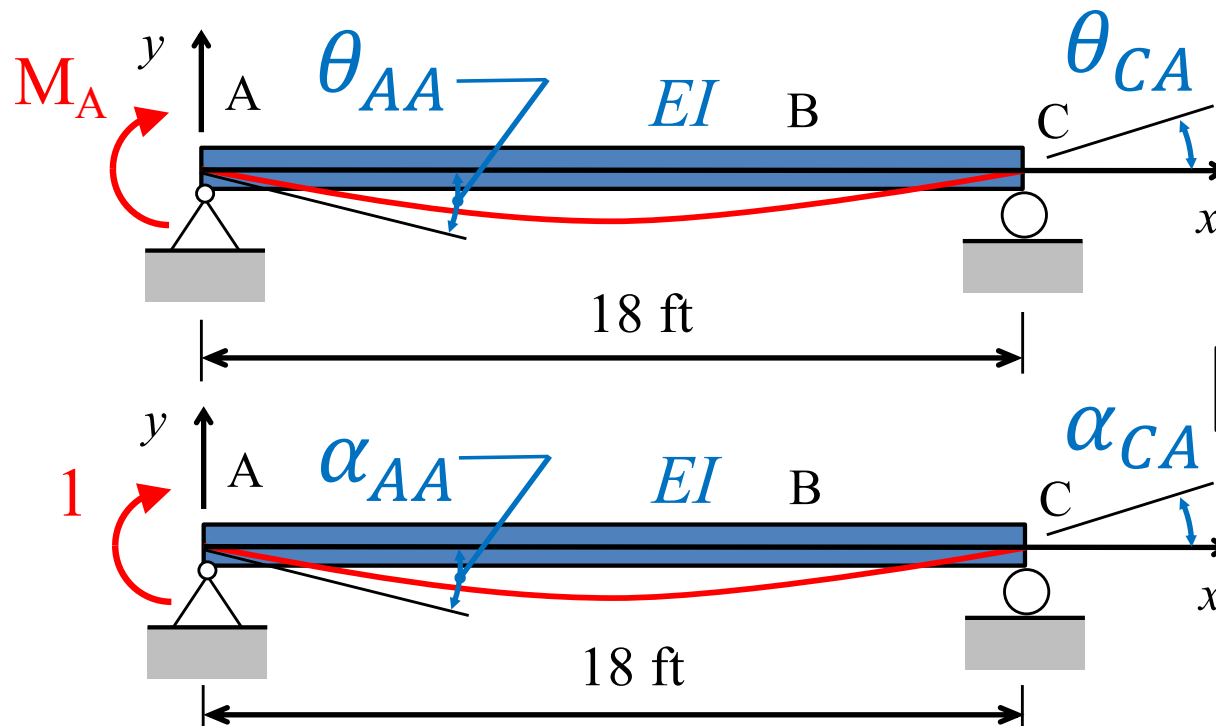
$$\theta \quad \curvearrowright +$$

## Simply Supported Beam Slopes and Deflections

Beam	Slope	Deflection	Elastic Curve
	$\theta_{\max} = \frac{PL^2}{16EI}$	$v_{\max} = \frac{-PL^3}{48EI}$	$v = \frac{-Px}{48EI} (3L^2 - 4x^2)$ $0 \leq x \leq L/2$
	$\theta_1 = \frac{Pab(L+b)}{6EIL}$ $\theta_2 = \frac{-Pab(L+a)}{6EIL}$	$v \Big _{x=a} = \frac{-Pba}{6EIL} \cdot (L^2 - b^2 - a^2)$	$v = \frac{-Pbx}{6EIL} (-x^2 - b^2 + L^2)$ $0 \leq x \leq a$
	$\theta_1 = \frac{ML}{3EI}$ $\theta_2 = \frac{-ML}{6EI}$	$v_{\max} = \frac{-ML^2}{\sqrt{243}EI}$	$v = \frac{-Mx}{6LEI} (x^2 - 3Lx + 2L^2)$ $0 \leq x \leq L$
	$\theta_{\max} = \frac{wL^3}{24EI}$	$v_{\max} = \frac{-5wL^4}{384EI}$	$v = \frac{-wx}{24LEI} (x^3 - 2Lx^2 + L^3)$ $0 \leq x \leq L$
	$\theta_1 = \frac{3wL^3}{128EI}$ $\theta_2 = \frac{-7wL^3}{384EI}$	$v \Big _{x=L/2} = \frac{-5wL^4}{768EI}$	$v = \frac{-wx}{384EI} (16x^3 - 24Lx^2 + 9L^3)$ $0 \leq x \leq L/2$ $v = \frac{-wL}{384EI} (8x^3 - 24Lx^2 + 17L^2x - L^3)$ $L/2 \leq x \leq L$
	$\theta_1 = \frac{7w_0L^3}{360EI}$ $\theta_2 = \frac{-w_0L^3}{45EI}$		$v = \frac{-w_0x}{360LEI} (3x^4 - 10L^2x^2 + 7L^4)$ $0 \leq x \leq L$

# Define and Solve the Redundant Problems

- There are the same number of redundant problems as degrees of indeterminacy;
- Define a reference coordinate system;
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- Calculate the flexibility coefficient associated with the relevant deflections for each redundant problem;



## Redundant Problem 1

$$\theta_{AA} = M_A \alpha_{AA}$$

$$\theta_{CA} = M_A \alpha_{CA}$$

## From Tabulated Solutions

$$\alpha_{AA} = ?$$

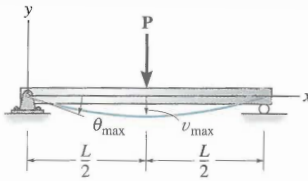
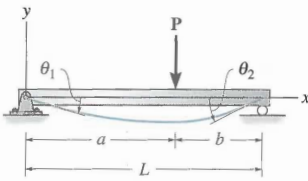
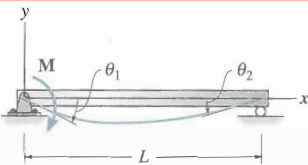
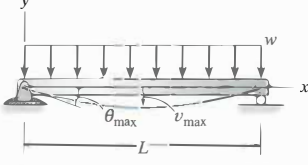
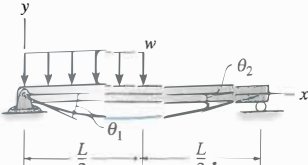
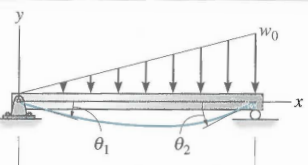
$$\alpha_{CA} = ?$$

# Tabulated Solutions

$v \quad + \uparrow$

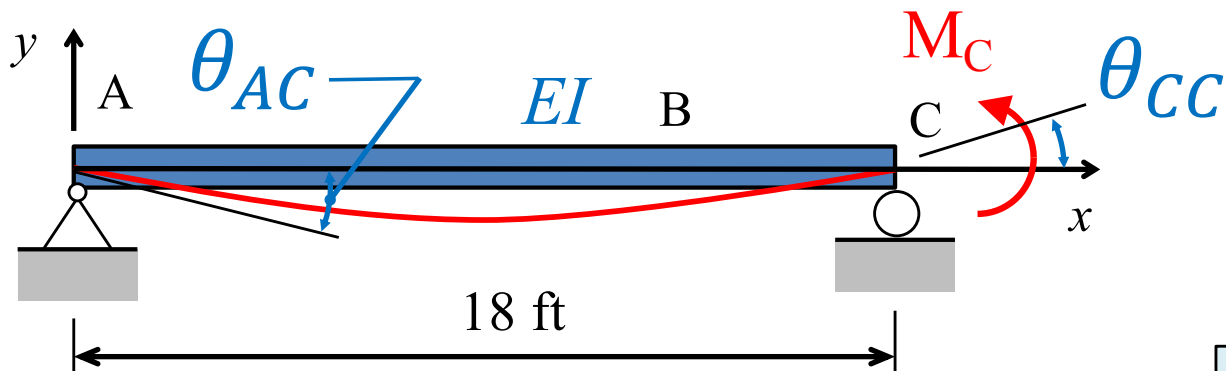
$\theta \quad + \curvearrowright$

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# Redundant Problem 2

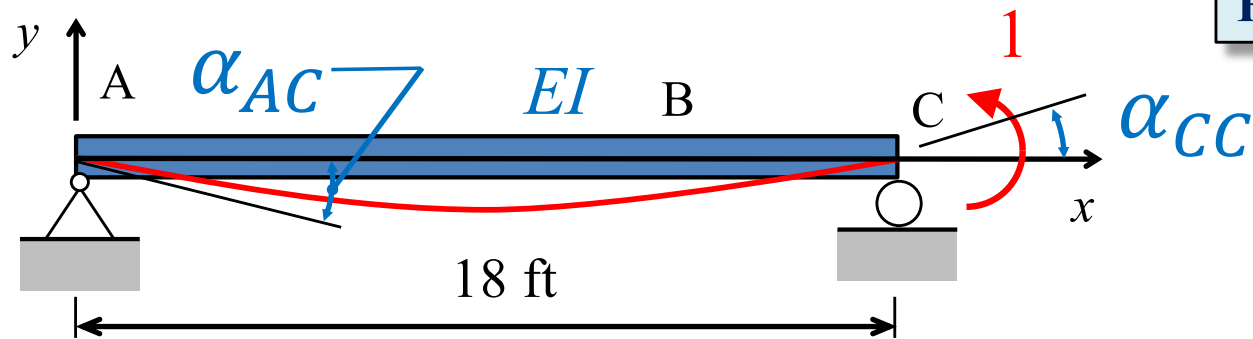
## Redundant Problem 2



$$\theta_{AC} = M_C \alpha_{AC}$$

$$\theta_{CC} = M_C \alpha_{CC}$$

## From Tabulated Solutions



$$\alpha_{AC} = ?$$

$$\alpha_{CC} = ?$$



# Compatibility Equation at Point A

## Compatibility at Point A

$$\theta_A + \theta_{AA} + \theta_{AC} = 0$$

## Compatibility Equation in terms of Redundant and Flexibility Coefficient

$$\theta_A + M_A \alpha_{AA} + M_C \alpha_{AC} = 0$$

# Compatibility Equation at Point C

## Compatibility at Point C

$$\theta_C + \theta_{CA} + \theta_{CC} = 0$$

## Compatibility Equation in terms of Redundant and Flexibility Coefficient

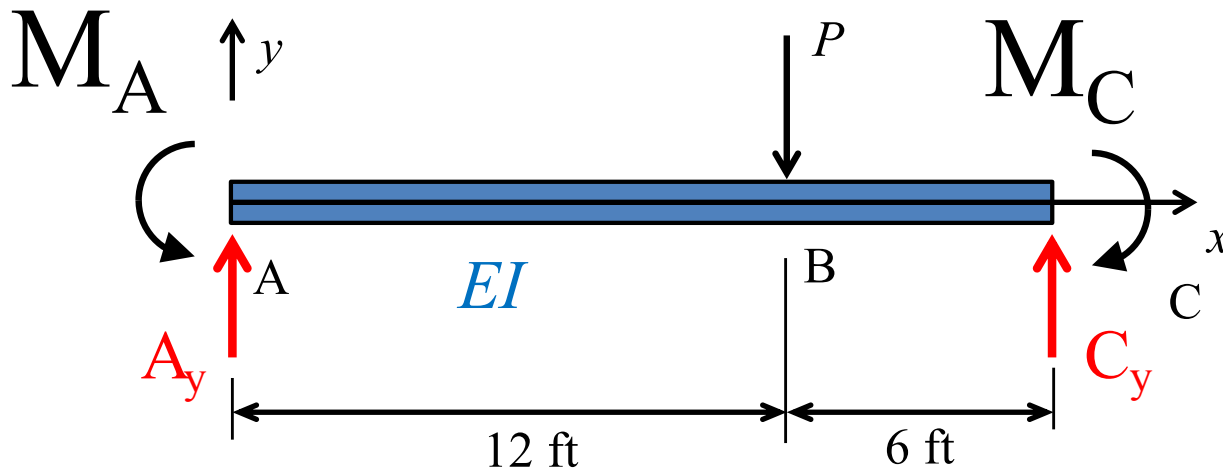
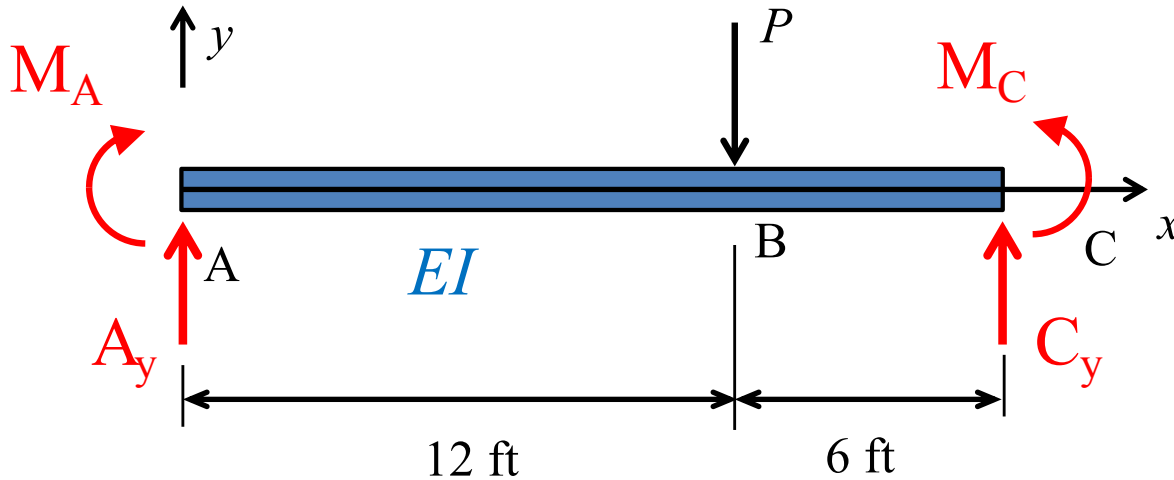
$$\theta_A + M_A \alpha_{CA} + M_C \alpha_{CC} = 0$$

## Solve Compatibility Equations for $M_A$ and $M_C$

$$\theta_A + M_A \alpha_{AA} + M_C \alpha_{AC} = 0$$

$$\theta_A + M_A \alpha_{CA} + M_C \alpha_{CC} = 0$$

# Free Body Diagram



Can now use equilibrium equations to find the remaining two unknowns